#### Reference (Axially Graded) Low Enriched Uranium Fuel Design for the HFIR

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# The goal of this presentation is to convince you that we're right

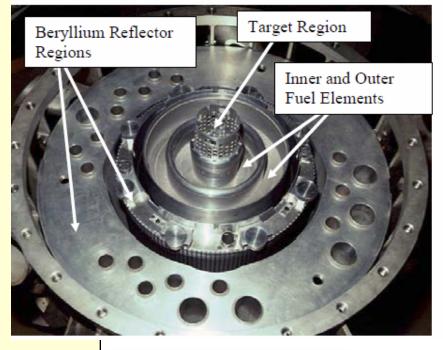
- Constraints that limited areas of study for HEU-to-LEU conversion
- The LEU fuel design
- Validity of physics studies
- Validity of thermal hydraulics studies
- Ability to fabricate LEU fuel

### Full paper will be posted on IGORR site



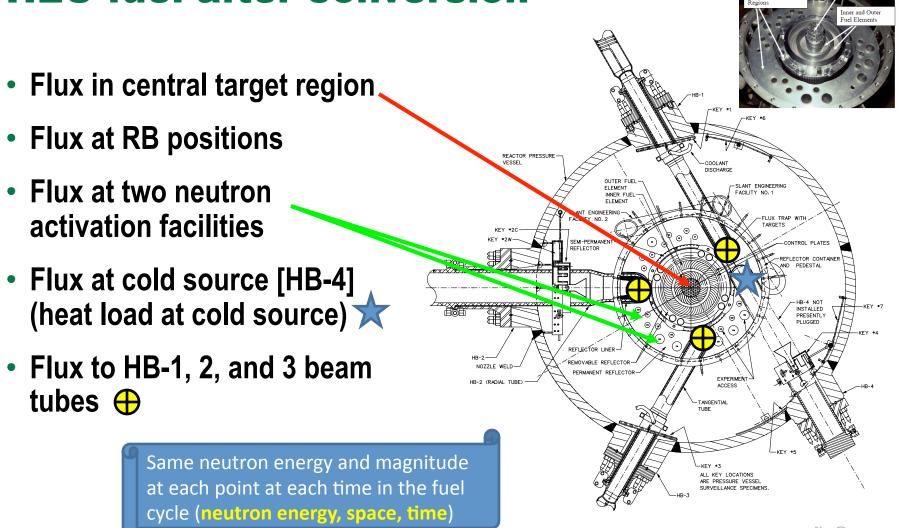
# Assumptions for HFIR LEU design studies were established and studies started in FY2006

- Build new reactor out of scope (\$)
- No changes to:
  - Physical dimensions tight
  - Geometry need Cf target
  - Al clad material or thickness testing
  - Fuel filler material (AI) testing
  - Fuel cycle length (~26 days) users
  - Margin of safety in TSR bases not less safe!
  - Coolant flow rate (no increase) major infrastructure
  - Subcriticality of elements handling, manufacture, transportation
  - Storage/handling methods major infrastructure
- Elements must "look the same"

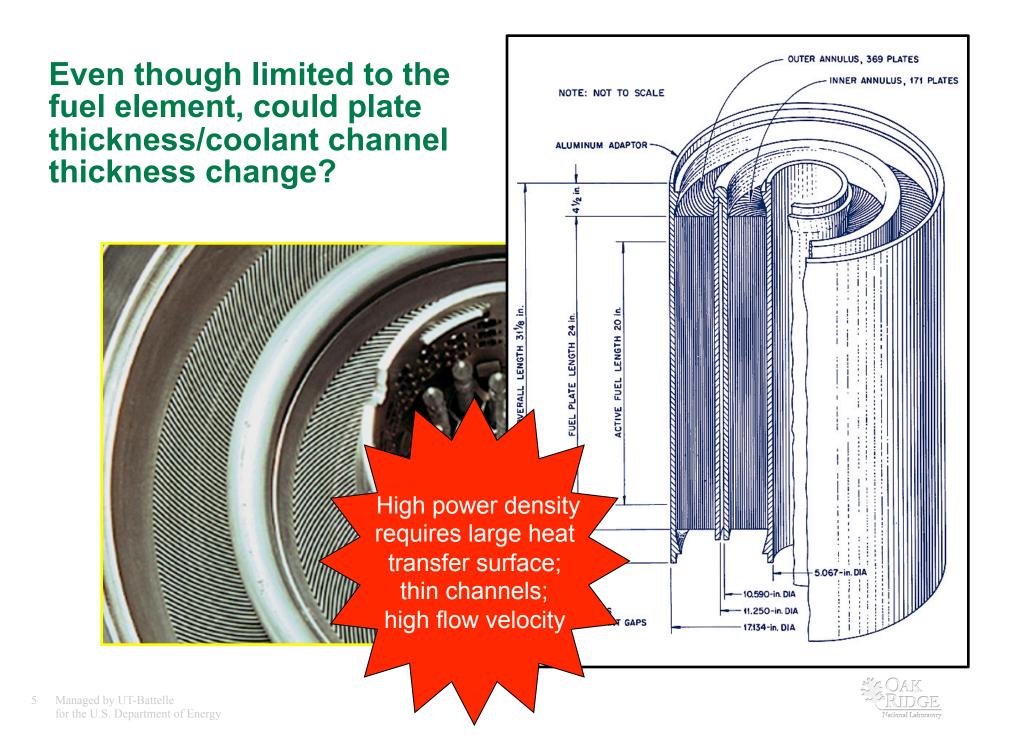




#### Flux performance goals are to retain the levels currently achieved at 85MW with HEU fuel after conversion



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# Only the interior of the fuel plates is changed – $U_3O_8/AI$ to U-10Mo

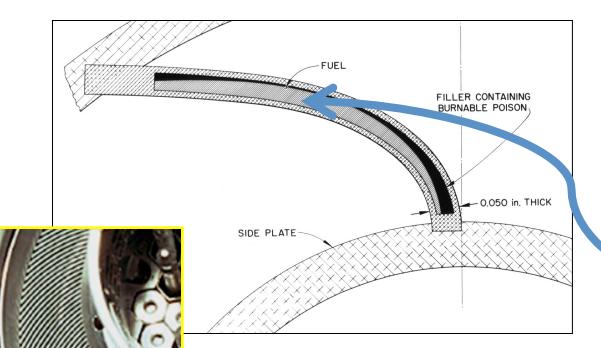




Fig. 15. Contouring the fuel section of the HFIR compact.

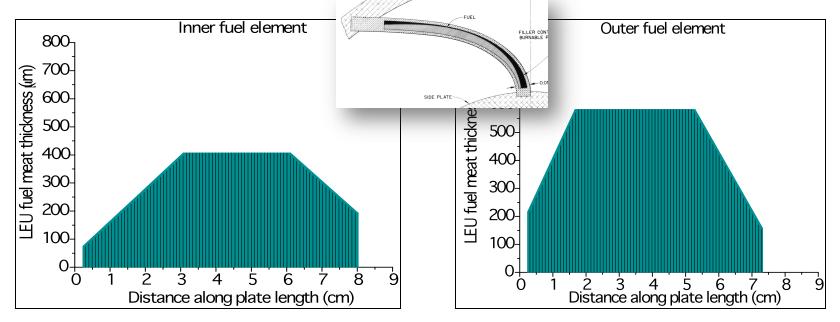
This "hand-formed" shape is unique to HFIR HEU fuel

- Monolithic graded LEU "foil" constraints
  - > ~75 micron minimum thickness
  - > ~750 micron maximum thickness





## **ORNL** staff have performed the neutronics and thermal hydraulics studies to design an LEU fuel





Uranium	Load (kg)
<sup>235</sup> U	25.2
<sup>238</sup> U	101.9
total	127.5

Future HFIR LEU fuel

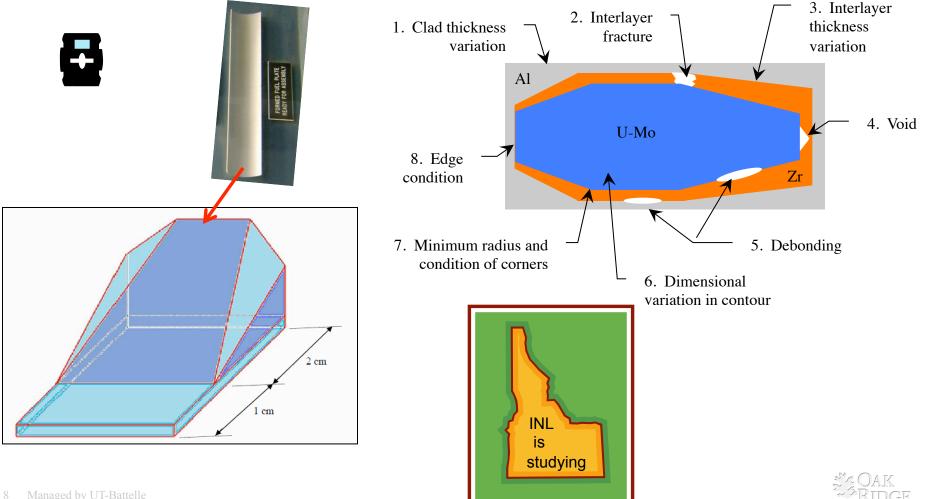
LEU fuel is much denser than HEU; LEU elements are 30% heavier.



# One technology change required – radial profile PLUS axial tapering of U-10Mo foil (U/Mo razor edge)

Shapes of bottom edges

of LEU plates



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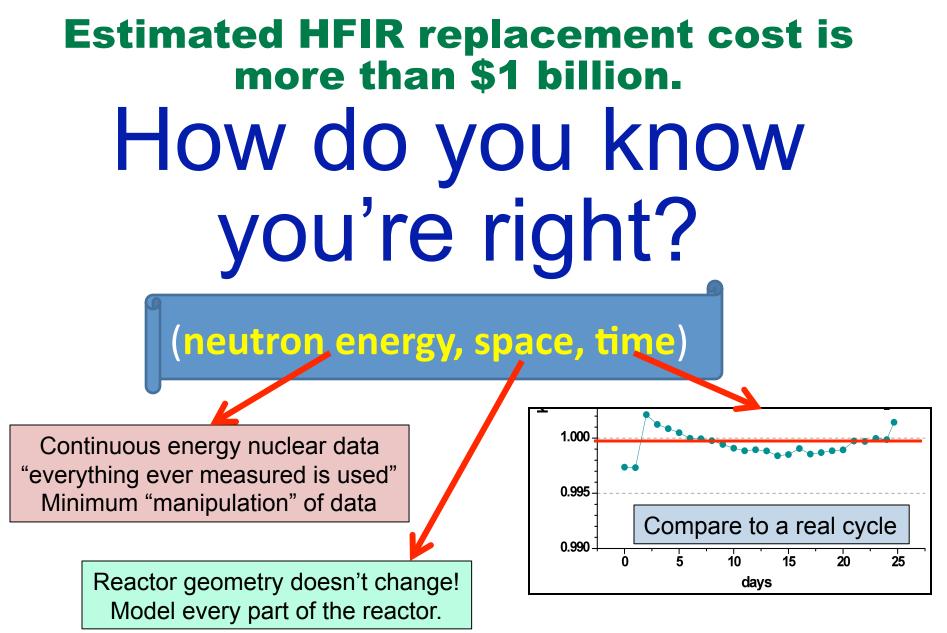
## LEU in HFIR is theoretically possible but requires a reactor power increase to 100 MW

### Showing parity to HEU performance requires examining several locations in the reactor; HEU at 85 MW, LEU at 100 MW

	Time	Fuel	Thermal flux (n/cm²s)	Epithermal flux (n/cm²s)	Fast flux (n/cm²s)	
Central target		HEU	2.2 × 10 <sup>15</sup>	$1.3 \times 10^{15}$	$1.1 \times 10^{15}$	Beryllium Reflector Cold Source
	BOC	LEU	2.3 × 10 <sup>15</sup>	$1.3 \times 10^{15}$	$1.1 \times 10^{15}$	
		HEU	2.3 × 10 <sup>15</sup>	$1.1 \times 10^{15}$	$1.0 \times 10^{15}$	
	EOC	LEU	2.5 × 10 <sup>15</sup>	$1.2 \times 10^{15}$	$1.0 \times 10^{15}$	
Cold source edge		HEU	$6.9 \times 10^{14}$	$2.4 \times 10^{14}$	$0.9 \times 10^{14}$	
	BOC	LEU	$8.3 \times 10^{14}$	$2.9 \times 10^{14}$	$1.0 \times 10^{14}$	Beam Tubes HB-3
		HEU	$8.4 \times 10^{14}$	$2.4 \times 10^{14}$	$0.9 \times 10^{14}$	
	EOC	LEU	$8.5 \times 10^{14}$	$2.8 \times 10^{14}$	$1.0 \times 10^{14}$	9
Reflector r=27cm		HEU	$6.0 \times 10^{14}$	$6.5 \times 10^{14}$	$4.1 \times 10^{14}$	(neutron energy, space, time)
	BOC	LEU	$7.1 \times 10^{14}$	$7.8 \times 10^{14}$	$4.8 \times 10^{14}$	
		HEU	8.1 × 10 <sup>14</sup>	$6.6 \times 10^{14}$	$4.0 \times 10^{14}$	
	EOC	LEU	7.4 × 10 <sup>14</sup>	7.5 × 10 <sup>14</sup>	$4.6 \times 10^{14}$	J" CAK

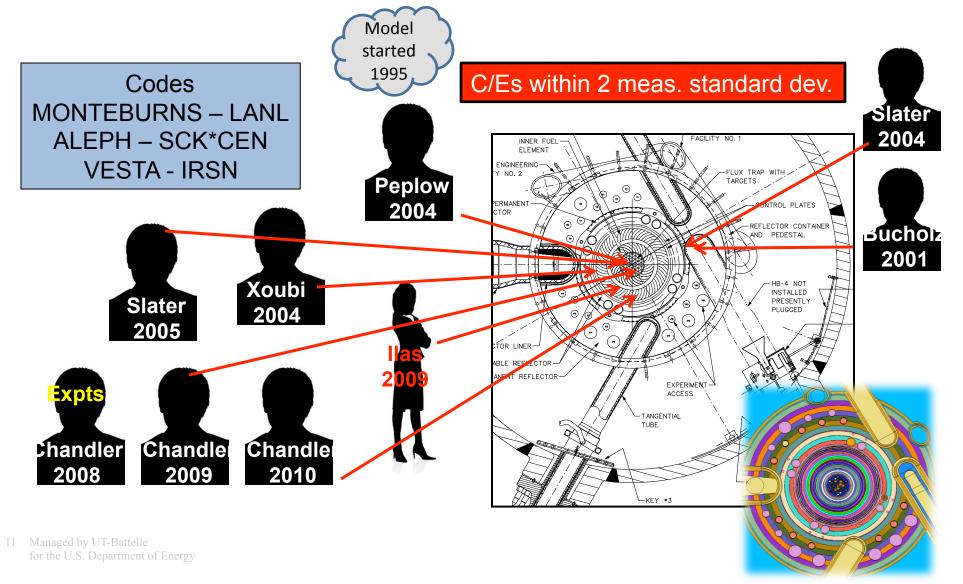
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# Years of validation studies with Monte Carlo (MCNP code) and Monte Carlo/depletion (MCNP/ ORIGEN) were performed with HEU data



## So what could go wrong?

- Significant quantity of molybdenum in reactor 12 kg (more Mo in LEU-fuelled HFIR than HEU today)
- Mo is a "mild" neutron absorber (10b to 100b)
- <sup>238</sup>U impacts 100 kg versus 0.7 kg
- Fast fissions in <sup>238</sup>U; fission product distribution differences; plutonium production

There is a lot of operating experience with 20% enriched fuel but everything happens faster in HFIR



# The thermal hydraulic analyses for LEU fuel are bounding not predictive

- LEU design uses 45-year-old HFIR HEU custom-written computer program
- Written to justify safety of HEU fuel, not performance as reactor physics does
- Models single inner element plate and channel and single outer element plate and channel (OK)



• Only models the heat flux from the plate surface and the water in the channel; goal is compute thickness of narrow channel (oxide growth, manufacturing tolerances, bowing, thermal deformation)

### The code "does not care" what fuel is inside the plate



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## So what could go wrong?

- Analyses based on HEU tolerances/uncertainties in specifications/measurements; what will LEU be?
- Differences in radiation induced phenomena (swelling)
- Thermally-induced deflection differences
- Flow induced effects? Not likely. U/Mo plate more rigid
- HFIR pressure, coolant velocity, clad material don't change

Our posture: Fuel development and fabrication tasks know the goals they must meet



## Each part of the U/Mo fuel fabrication process seems well-known



a) Health Physics Research Reactor fuelled with U-10Mo alloy



b) Contoured rolling of U/Mo foil



c) Placing "Razor" edge on bottom of U/Mo foil



d) Fabricate thin Zr foil for diffusion barrier



e) Borated Al for inner plate



f) Hot isostatic pressing of U/Mo, Zr, Al clad and borated Al if inner plate



g) Since U/Mo foil is contoured, top of pressed plate must be machined to be flat



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### So what could go wrong?

- Bonding; in the HIP process and subsequent forming to involute shapes
- Measurement techniques/uncertainties
- Robustness (variation) of fabrication process; repeatability
- Can the pieces be put together?
- Cost

Our posture: Fabrication knows the goals they must meet but feedback to design process is still possible



# With methods reported here, additional analyses offer diminished returns unless new information made available

- Rather than analyses, need data, data, data
- ATR fuel development tests
- Fabrication process development tests
- Instrumentation
- One exception better thermal hydraulics analyses (subject of later talk by Dr. Jim Freels)
- Communication with other reactors as they convert (HFIR last)



# **Convinced?**

Questions/ comments welcome

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